

Injection and Kicker

IPNS review
List in CM26

- Requirement from physics analysis
- Requirement for VBO.¹
 - Residual kicker field.¹



- Beam orbit design
- **Possible improvement**^{3,5}
 - ASSM
 - **Vacuum vessel wall**
 - **Tuning strategy**^{2,17,22,3}
 - **Required precision estimation**
 - **Monitor design**
 - Transient analysis (incl. E-field)^{25,6}
 - Beam transport in yoke tunnel.^{16,21,6}
 - Instability in real experiment²
 - Instability in beam
 - Instability in kicker pulse



- Kicker coil design⁴
- Insulation for $\pm 40\text{kV}$ incl. feedthrough
 - Pulse power supply
 - Mechanical support (for hoop stress)

Abe,
Takayanagi



- Demonstration of design
- Rotatable QM²⁰
 - Prototype of power supply^{2,23}
 - Prototype kicker coil²
 - Test bench of spiral injection¹⁸

Matsushita

Possible improvement

I put the 1st priorities

- What is the better coil shape?
- Why we pick such selection, what philosophy?

Because;

- To estimate ASSM/ASQM requirement
- To continue kicker coil's design (tangent current, noise or mechanical shape,..)
- To confirm required X-Y coupling is independent on kicker coil (I know from the experience, but I hadn't confirmed it)
- To give beam track information for beam monitor designing

I will discuss why "typ31ME" is the better one from the others.
Ogawa-san is also confirmed what is the better one among candidates.

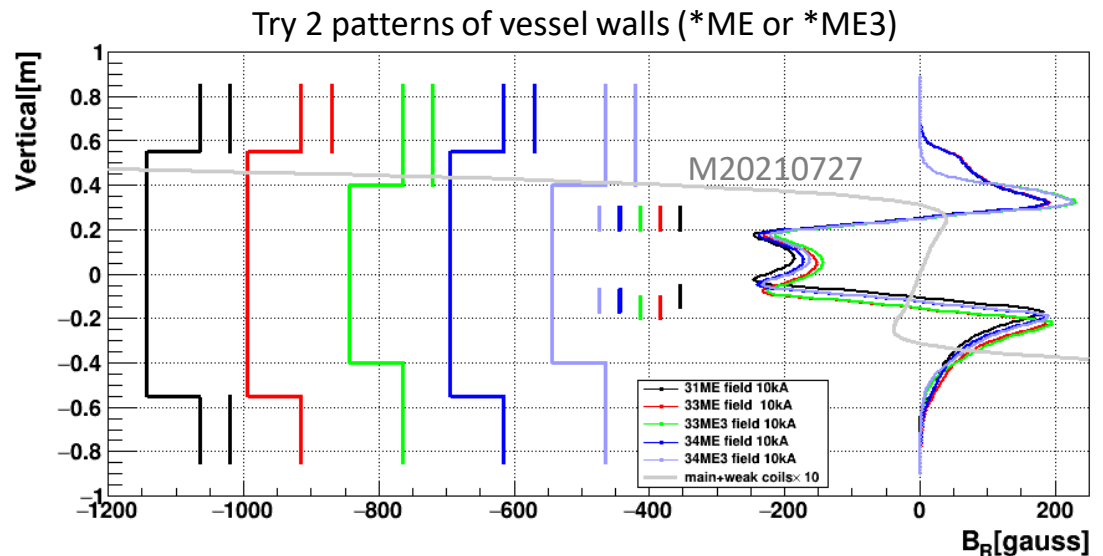
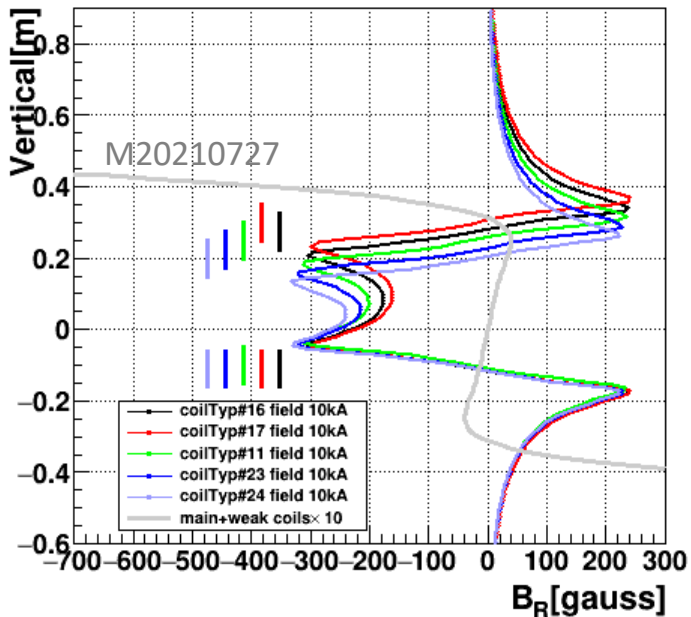


表 キッカーコイル候補案のCoil配置(2021/12/17~2022/06/17)

No.	下コイル			上コイル			電流分布	BR (Gauss) R=0.333m					インダクタンス	判定	Fz (N) (電流方向未確認)	発熱 (W)	電流 (A)	備考
	幅 (mm)	中心 R(mm)	中心 Z(mm)	幅 (mm)	中心 R(mm)	中心 Z(mm)		Z=0.20	Z=0.10	Z=0.05	Z=0.0	Z=-0.05						
0	1.0	350	-56	1.0	350	+300	平坦	11.93	9.44	11.47	18.35	20.47	6.11μH	6.53				
1	100	350	-105	100	350	+350	両端Peak	8.359	6.999	8.152	11.62	16.23	2.08μH			0.036		
2	50	350	-80	50	350	+350	両端Peak	8.284	7.528	9.150	13.78	23.17	2.66μH			0.063		
3	3	350	-56.5	3	350	+350	平坦分布(仮想)						5.11μH		×	0.675		
4	100	350	-105	100	350	+350	平坦分布(仮想)						2.14μH			0.02		
5	100	355	-110	100	355	+350	両端Peak	8.274	6.881	7.892	10.83	16.22	2.12μH	16.48		300	基準案 6.7kV	
6	100	355	-110	100	425	+350	両端Peak	6.691	6.797	7.958	10.96	16.37	2.14μH		×			
7	50	355	-80	50	355	+350	両端Peak	8.291	7.554	9.128	13.48	19.04	2.71μH	15.37				
8	100	355	-110	100	355	+450	両端Peak	5.098	5.578	6.969	10.15	15.70	2.19μH		×			NG
9	100	355	-110	100	355	+250	両端Peak	14.82	10.09	9.863	12.17	17.19	2.00μH					
10	30	333	-70	100	355	+350	SQ平坦分布	8.471	7.410	8.885	13.21	30.99	2.14μH		×	195	4.4kV	
11	100	360	-100	100	360	250	両端Peak	13.38	10.33	10.33	12.94	13.38	2.021μH	18.13				
12	100	360	-100	100	360	350	両端Peak	8.379	7.187	8.373	11.59	12.49	2.146μH	15.12		+1.000		
13	100	360	-100	100	360	450	両端Peak	5.246	5.878	7.441	10.90	11.99	2.225μH					
14	100	360	-110	100	360	350	両端Peak	8.308	7.041	8.118	11.08	13.60	2.151μH	15.19				基準案(2022/04/12)?
15	100	360	-110	100	360	250	両端Peak	13.26	10.05	9.839	11.95	15.22	2.036	18.16		-0.743		
16	100	360	-110	100	360	275	両端Peak	14.78	8.923	9.181	11.51	14.92	2.072	17.18				
17	100	360	-110	100	360	300	両端Peak	12.02	8.079	8.657	11.16	14.66	2.103	16.39		-0.492		
18	100	360	-110	100	360	325	両端Peak	9.798	7.425	8.232	10.86	14.45	2.131	15.73		+0.263		
19	100	360	-110	100	360	375	両端Peak	7.130	6.482	7.580	10.40	14.11	2.178					
20	100	360	-110	100	360	400	両端Peak	6.291	6.134	7.343	10.22	13.97	2.198	14.35		+4.989		
21	100	360	-110	100	360	425	両端Peak	5.641	5.844	7.134	10.06	13.85	2.215					
22	100	360	-110	100	360	450	両端Peak	5.124	5.599	6.954	9.922	13.76	2.231	13.72		+12.779		
23	100	360	-110	100	360	225	両端Peak	5.554	11.70	10.76	12.58	15.66	2.025	19.34		-0.685		2022/04/27追加
24	100	360	-110	100	360	200	両端Peak	1.201	11.92	11.92	13.26	16.11	1.978	21.20		-0.595		2022/04/27追加
25	100	360	-110	200	380-400	300	両端Peak	7.315	8.358	9.012	11.54	14.87	1.801	19.67		-0.012		2022/05/24追加
26	100	360	-110	200	380	220	両端Peak	1.583	11.13	11.72	13.33	16.09	1.666	24.71		-0.745		dBr/dz > 0の部分が導体間に存在しない。
27	100	360	-110	150	380	200	両端Peak	0.993	11.98	12.09	13.60	16.34	1.771	23.72		-0.680		
28	100	360	-103	100	360	250	両端Peak											2022/06/17
29	100	360	-105	100	360	250	両端Peak											
30	100	360	-107	100	360	250	両端Peak											

表 キッカーコイル候補案のCoil配置(Type-11, 11M, 11ME, 31, 31M, 31ME案)

No.	下コイル			上コイル			電流分布	BR (Gauss) R=0.333m					インダクタンス	単純平均BR	Fz (N) (真空容器-Main Coil)	発熱 (W)	電流 (A)	備考 真空容器電流
	幅 (mm)	中心 R(mm)	中心 Z(mm)	幅 (mm)	中心 R(mm)	中心 Z(mm)		Z=0.20	Z=0.10	Z=0.05	Z=0.0	Z=-0.05						
11	100	360	-100	100	360	250	両端Peak	13.45	10.43	10.43	13.08	13.46	2.021μH	12.17		± 500		
11M	100	360	-100	100	360	250	5mm厚導体	12.73	10.45	10.43	12.94	12.79	2.030μH	11.99		± 500		
11ME	100	360	-100	100	360	250	5mm厚導体	12.31	9.74	9.76	12.29	12.28	未計算	11.26	2.05N	± 500	23.63A	
31	100	370	-100	100	370	250	両端Peak	11.15	10.28	10.28	12.24	11.16	2.147μH	11.02		± 500		
31M	100	370	-100	100	370	250	5mm厚導体	10.62	10.27	10.26	12.07	10.68	2.096μH	10.78		± 500		
31ME	100	370	-100	100	370	250	5mm厚導体	10.17	9.52	9.54	11.40	10.17	未計算	10.16	1.90N	± 500	23.71A	

Vacuum vessel wall models:

Typ31ME,

Typ31ME2~typ31ME5

typ33ME,typ33ME3,

typ34ME,typ34ME3

Table Parameters for Kicker field conceptual design (+/- 500A)

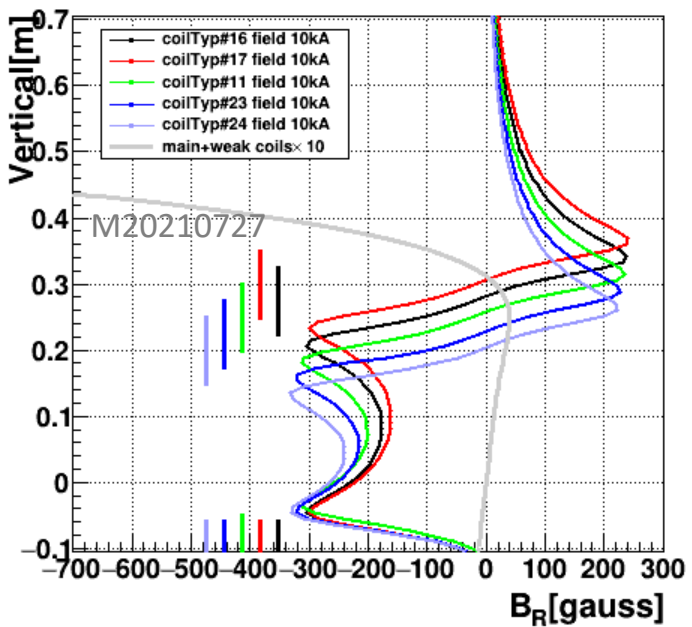
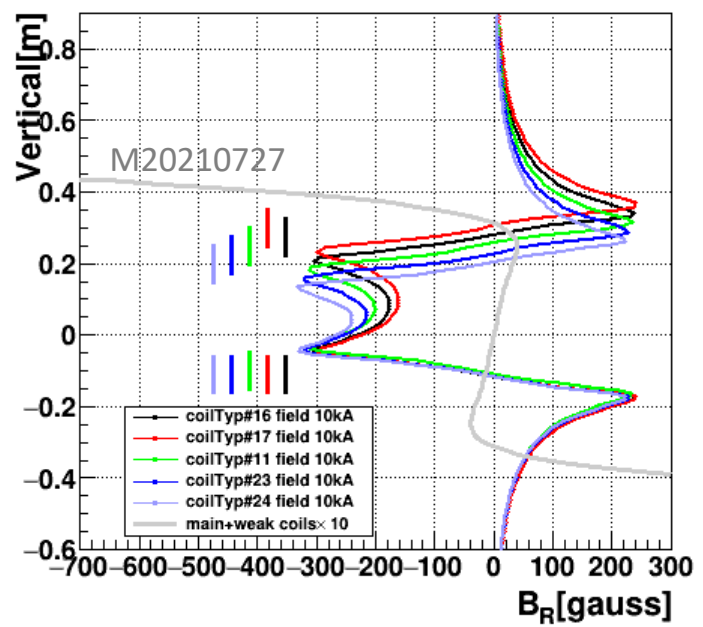
Parts	Parameter	Meaning	Type- →	31ME	31ME-2	31ME-3	31ME-4	31ME-5	33ME	33ME-3	34ME	34ME-3
Duct & Vessel wall	DZHI	Beam duct end height (Inner)	0.550	0.4750	0.400	0.600	0.400	0.550	0.550	0.400	0.550	0.400
	DZHO	Beam duct end height (Outer)	0.550	0.4750	0.400	0.600	0.550	0.550	0.400	0.550	0.400	0.400
	VZH	Vertical height of vessel ceiling	0.550	0.4750	0.400	0.600	0.550	0.550	0.400	0.550	0.400	0.400
	RD	Inner radius of beam duct	0.412	0.412	0.412	0.412	0.412	0.412	0.412	0.412	0.412	0.412
	RW	Outer radius of beam duct	0.300	0.300	0.300	0.300	0.300	0.300	0.300	0.300	0.300	0.300
	Coil conductors	CZtop	Z height of top coil center	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250
CZbot		Z height of bottom coil center	-0.100	-0.100	-0.100	-0.100	-0.100	-0.100	-0.150	-0.150	-0.120	-0.120
半径方向磁場BR強度	B333+175	R=0.333, Z=0.175mのBR	12.23	12.00	11.40	12.30	11.78	11.54	10.67	11.92	11.07	
	B333+050	R=0.333, Z=0.050mのBR	9.54	9.44	9.13	9.59	9.35	7.65	7.19	8.67	8.23	
	B333-0	R=0.333, Z=0.0mのBR	11.39	11.31	11.06	11.43	11.26	8.35	7.97	10.04	9.67	
	B333-050	R=0.333, Z=-0.050mのBR	10.17	10.15	9.96	9.59	10.12	10.56	10.22	11.97	11.65	

赤字数値はType-31MEのものである。Type-32はCZtopを0.29mとしたもので既提示、表中の数値の単位はm
 コイル導体は5mm幅、10cm高さで、端部は2.5mm半径円弧の形状、上表では中心位置を変更している
 31MEでは下側コイルの中心CZbotは-0.100m、33MEは下側コイルの中心をCZbot=-0.15m、34MEではCZbot=-0.120mとした。
 33MEに比べ34MEでは蓄積領域のBRが強い。33MEでは、BR成分が弱くなっている。

Try typical five types of coil shapes typ11,16,17,23,24 (change upper coil's position)

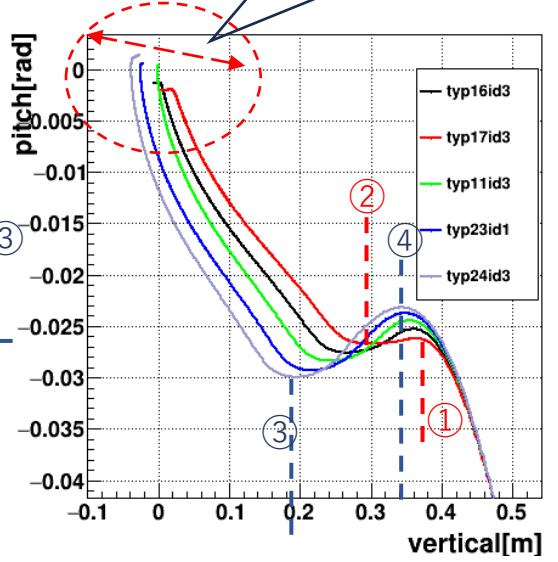
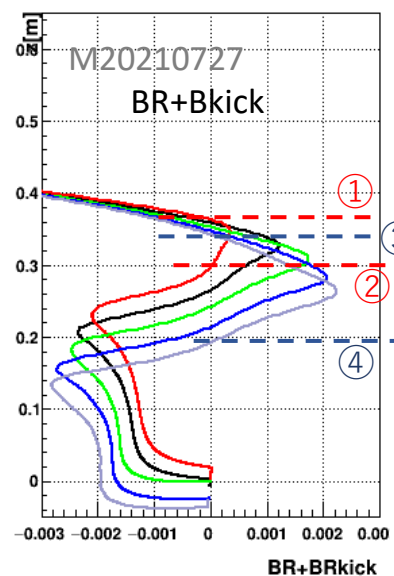
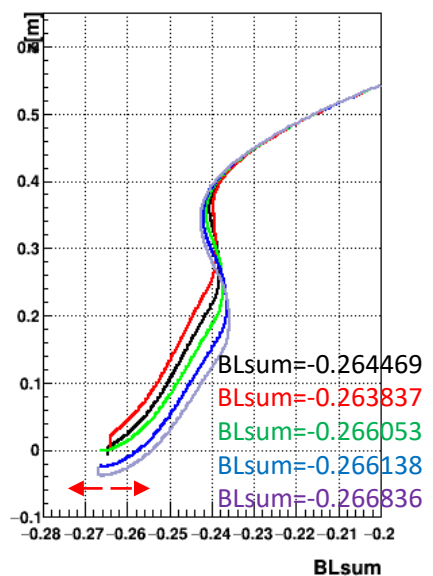
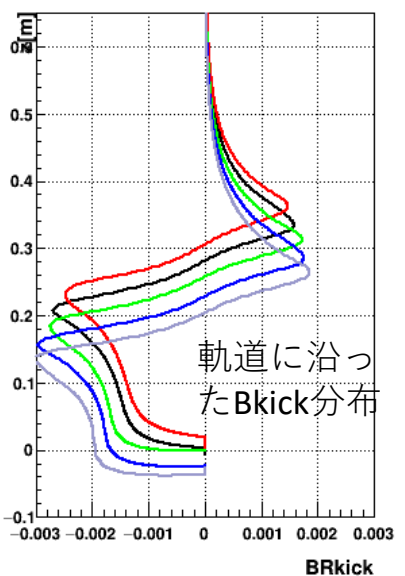
キッカーコイルタイプ (真空槽なし) typ16,17,11,23,24 について

各コイルにTyp11のキッカーパラメータ (電流、時間) を与え、同じ入射条件 (typ11の座標、角度) で軌跡を比較



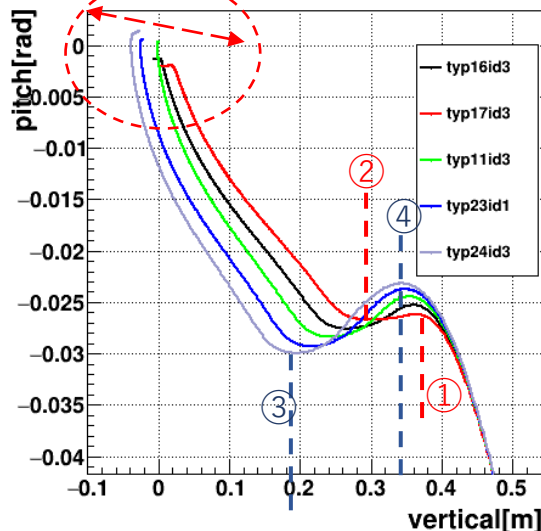
Coil#	Up [mm]	Down [mm]
16	275	-100
17	300	-110
11	250	-110
23	225	-110
24	200	-110

Residual z and z' differs



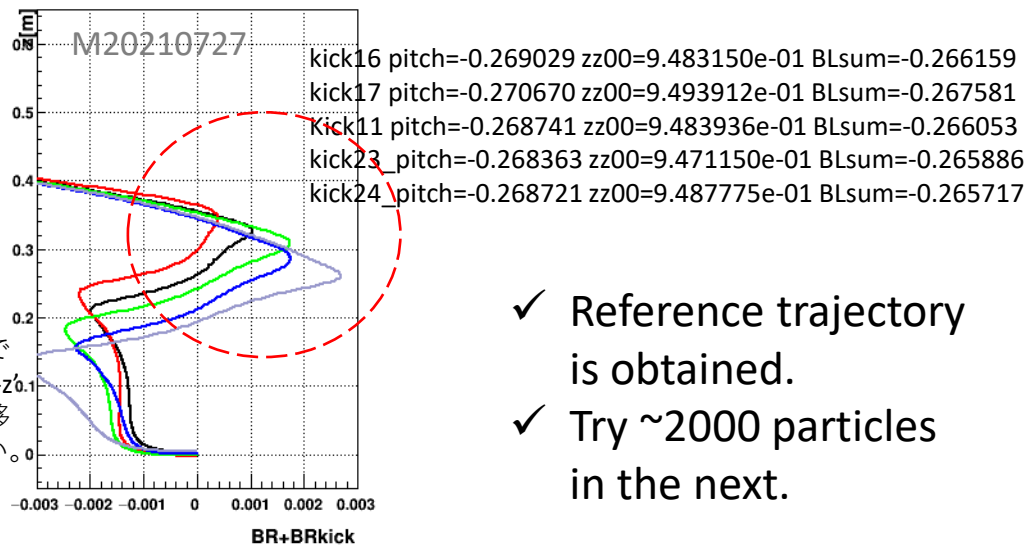
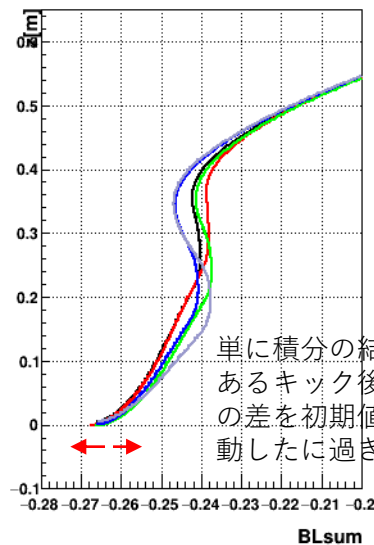
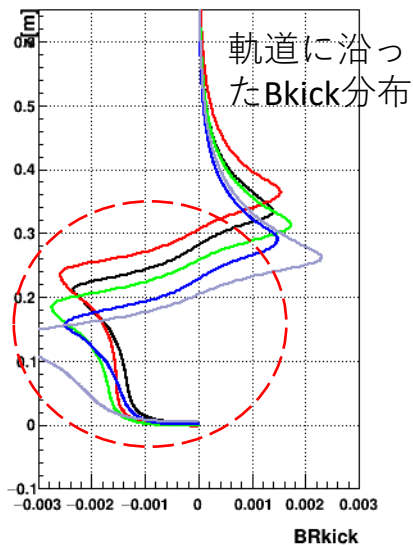
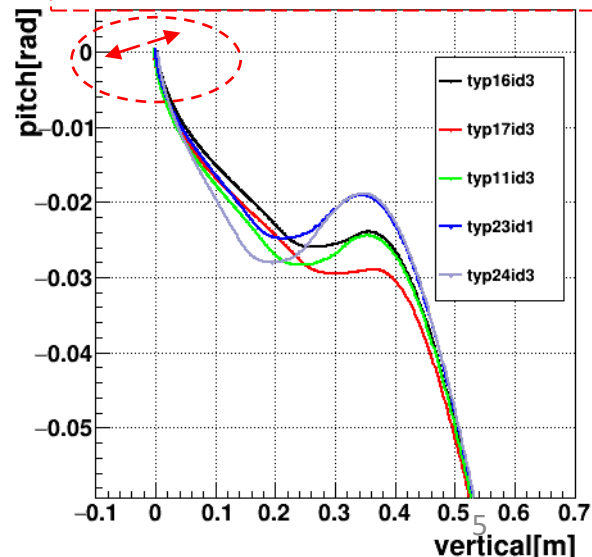
Adjust each reference trajectory by changing pitch angles and vertical positions at $z \sim 0.95\text{m}$ to minimize residual z and z' at the end of the kick.

Residual z and z' differs



キッカーコイルタイプ（真空槽なし）typ16,17,11,23,24 について各コイルに個別のキッカーパラメータを与え、個別入射条件（座標、角度調整）でキック後の $z-z'$ が 0-0 に近づくよう調整した軌道と比較

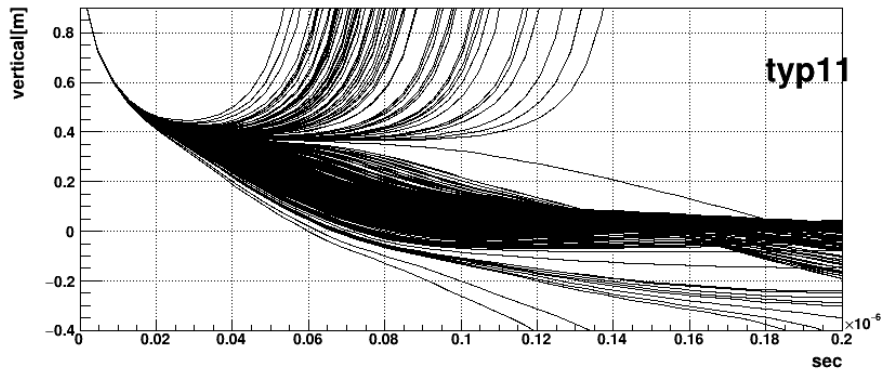
入射ビームのパラメータ（座標、方向）を微調した結果、BLsumの分布を近いまま、 $z-z'$ の終点をそろえることができた。



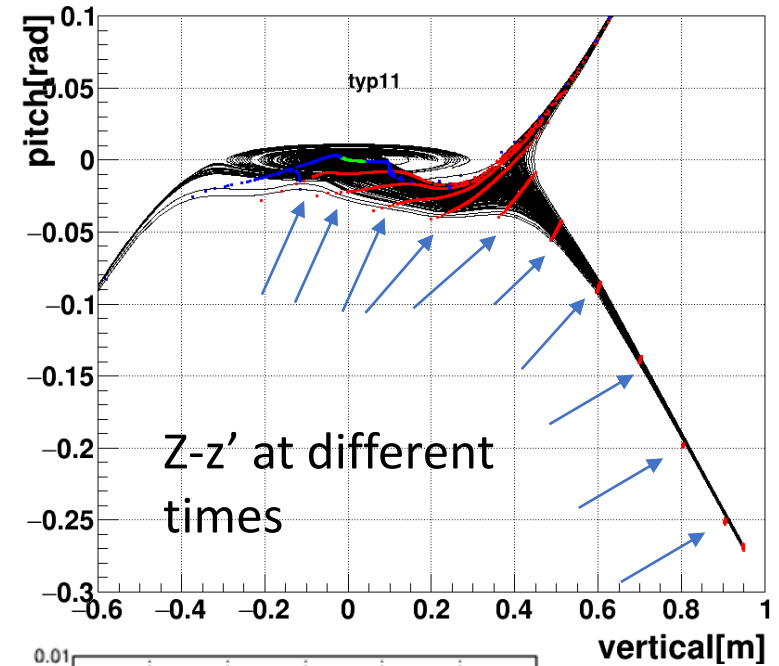
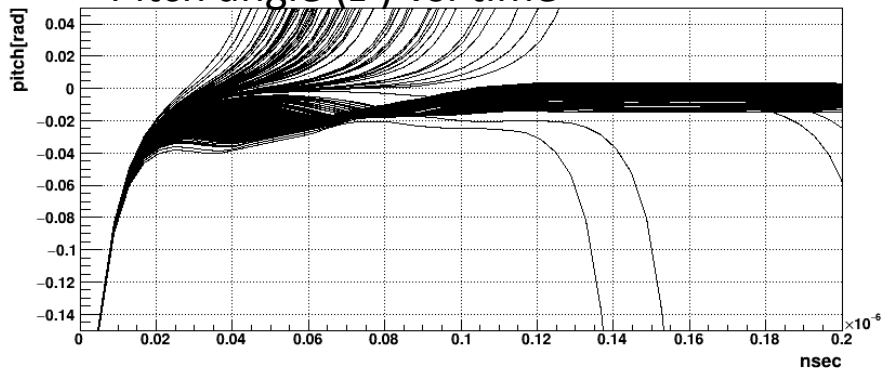
- ✓ Reference trajectory is obtained.
- ✓ Try ~ 2000 particles in the next.

Try ~ 2000 particles

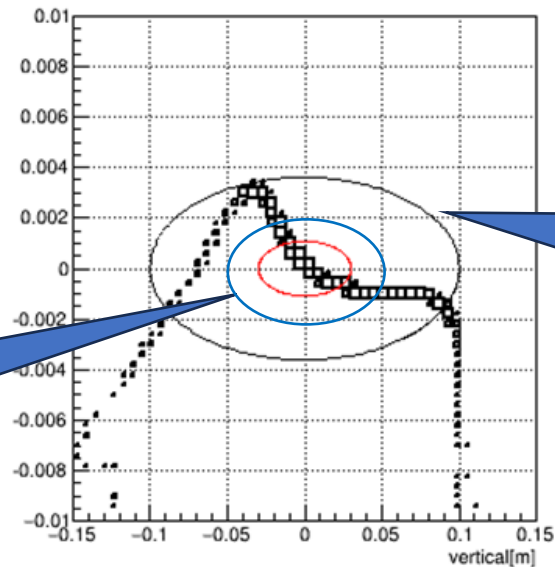
Vertical position (z) vs. time



Pitch angle (z') vs. time

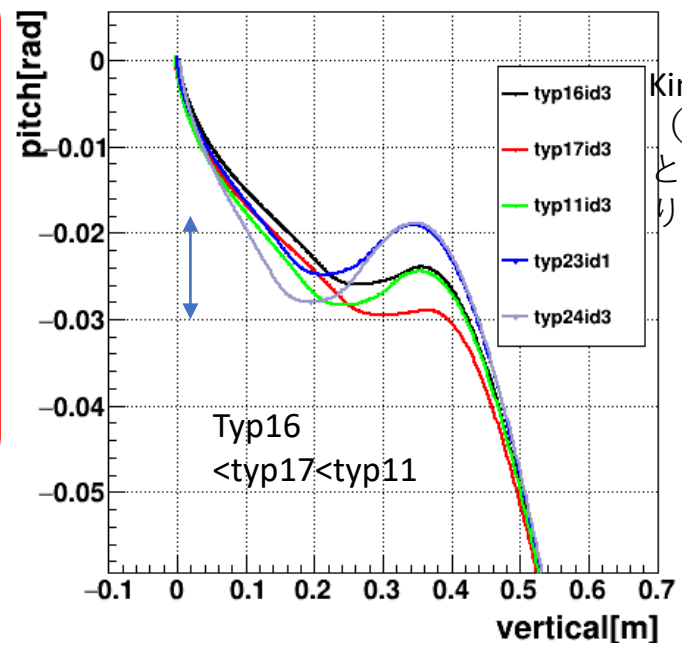
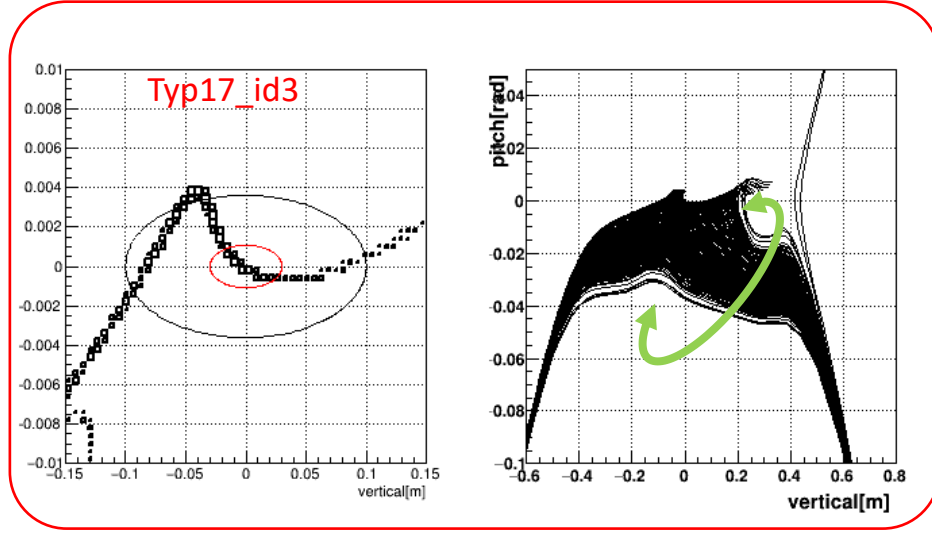
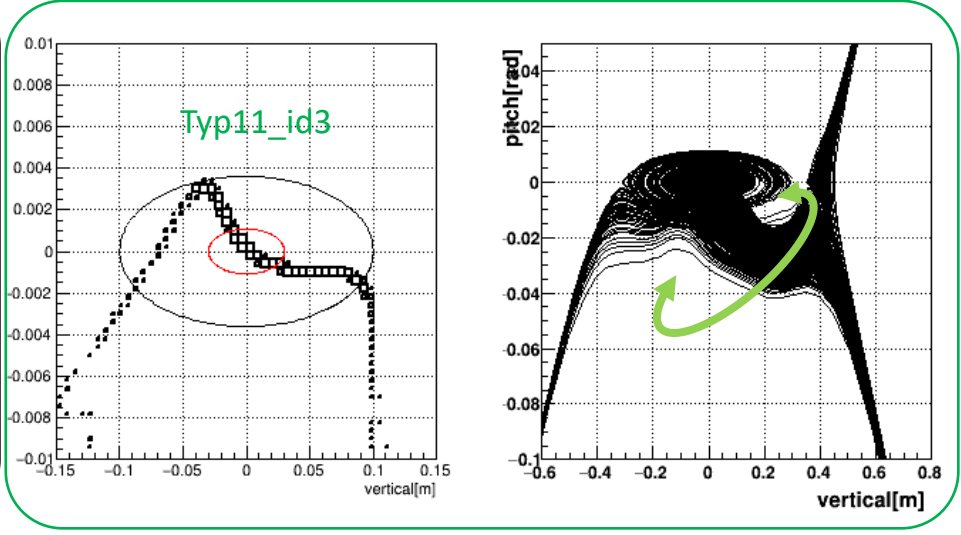
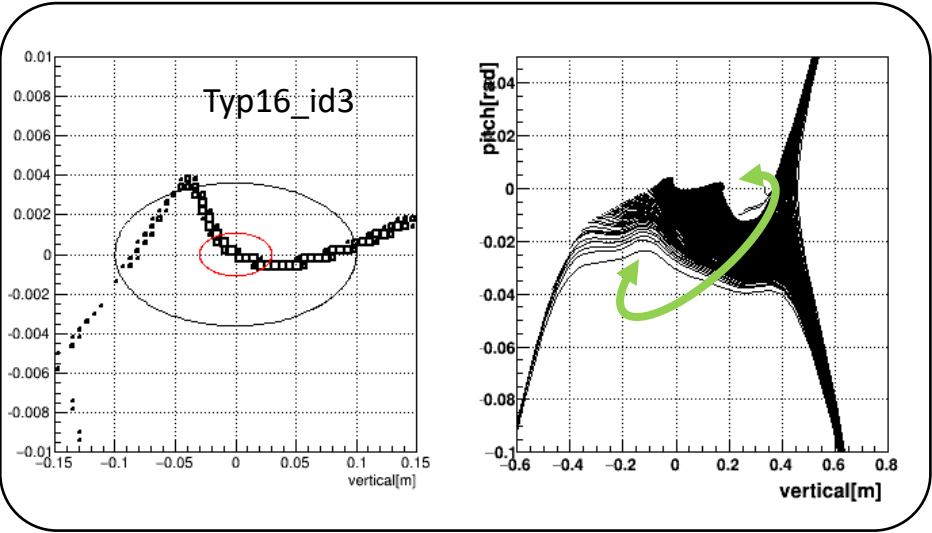


Z-z' at different times



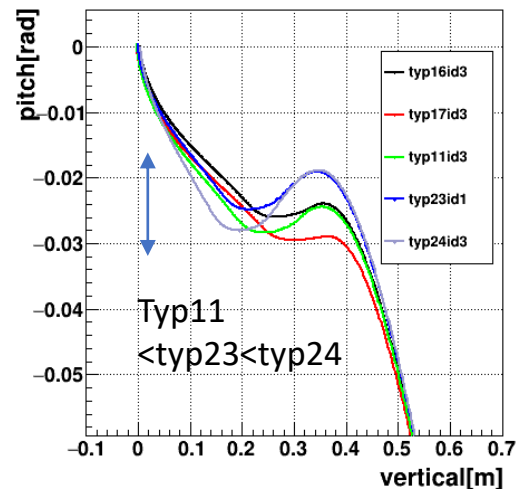
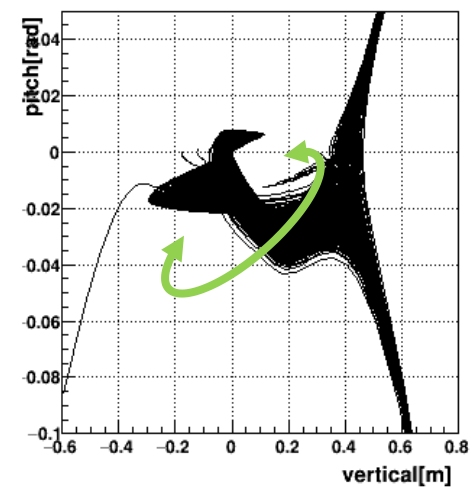
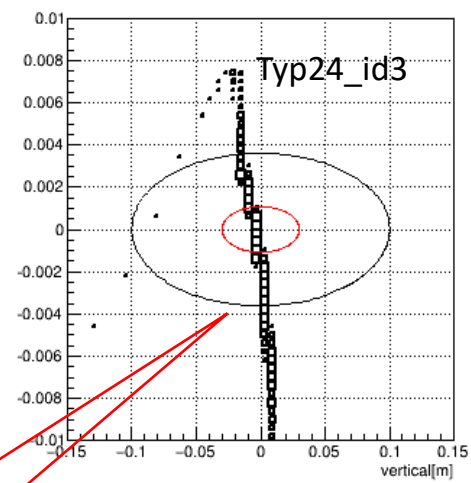
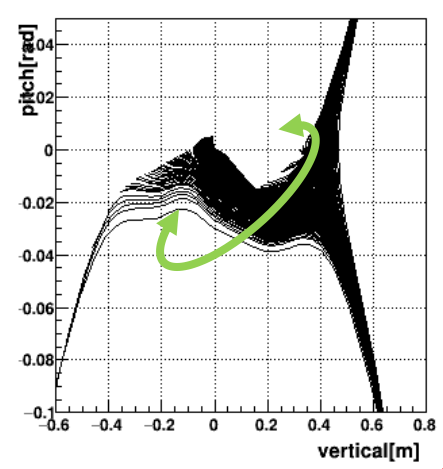
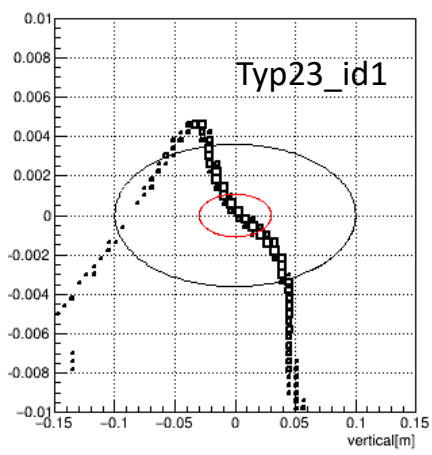
Weak focus' ellipse

Trajectories with in $|z| < 0.05$ m ellipse, is stored appropriately.



Kinkの振幅が小さい
(収束が小さい)
と、ビームの広がり
が大きい

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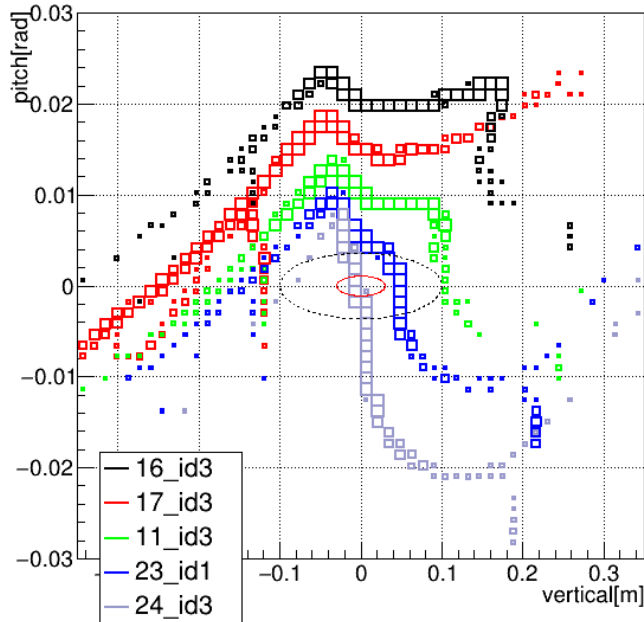
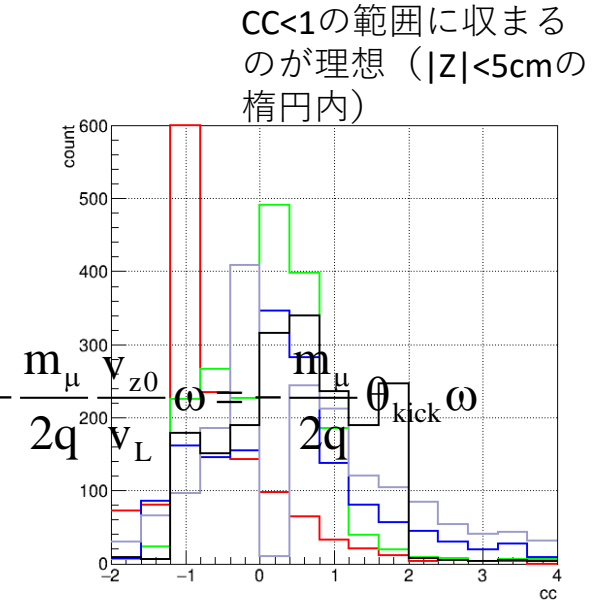
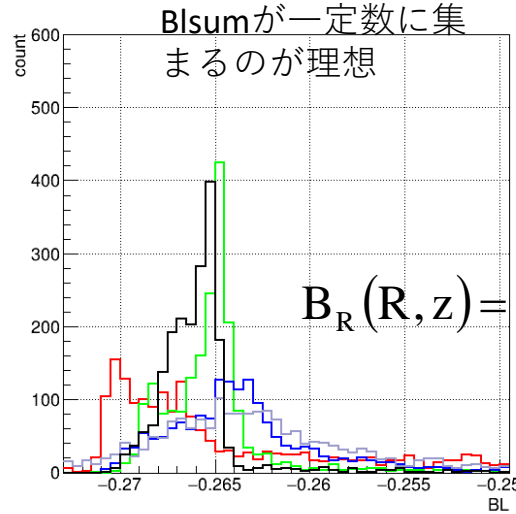
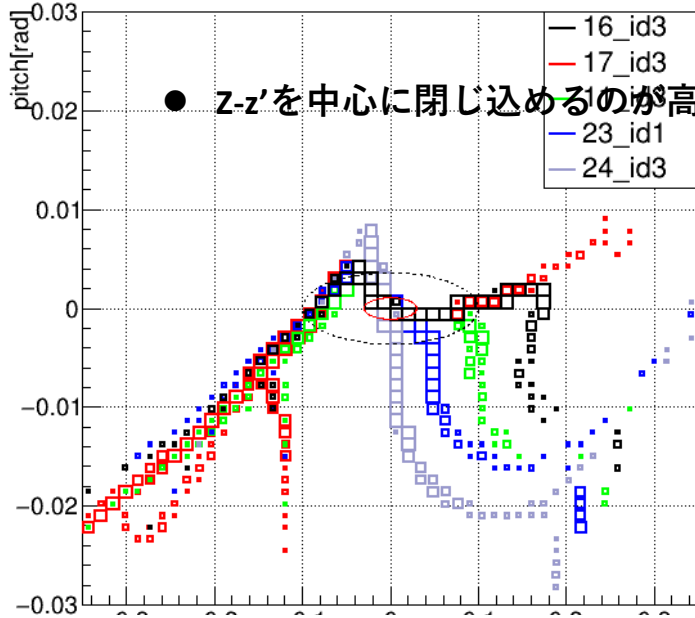
Kinkの振幅が大きい
(収束が大きい)と、
ビームの広がりが小さいが、 $z-z'$ が立ち z'
の広がりを制御できない。
(typ24_id3)

	Up/	Low	$ z < 0.05$	ΣBL_rms
Typ16_id3	275	-100	0.30	0.0025
Typ17_id3	300	-110	0.14	0.0083
Typ11_id3	250	-110	0.42	0.0031
Typ23_id1	225	-110	0.29	0.0051
Typ24_id3	200	-110	0.26	0.0061

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z-z' at the end of the kick & ΣBL

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$$B_R(R, z) = -\frac{m_\mu}{2q} \frac{v_{z0}}{v_L} \omega = -\frac{m_\mu}{2q} \theta_{kick} \omega$$

$$v_z(t) = v_{z0} + \frac{q}{m_\mu} v_L B_R(R, z) \int \sin(\omega \times t) dt$$

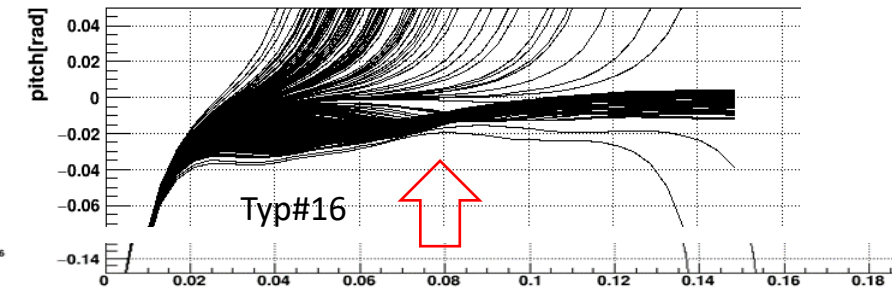
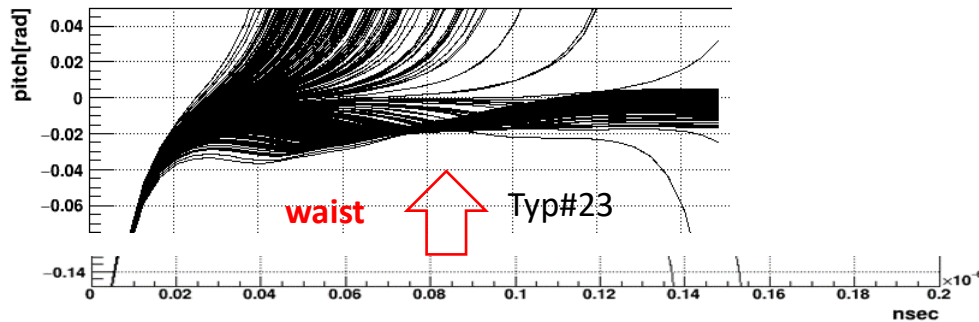
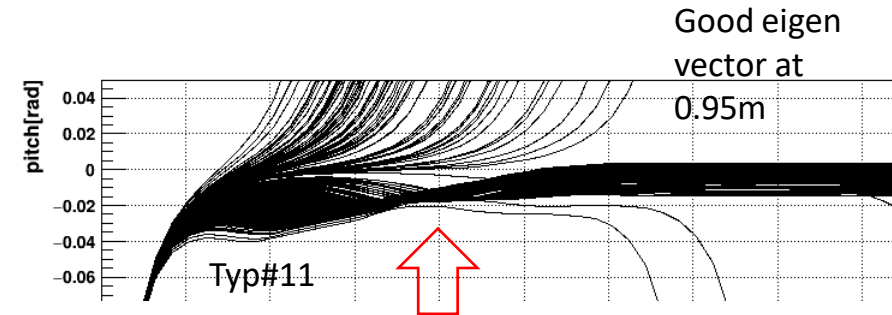
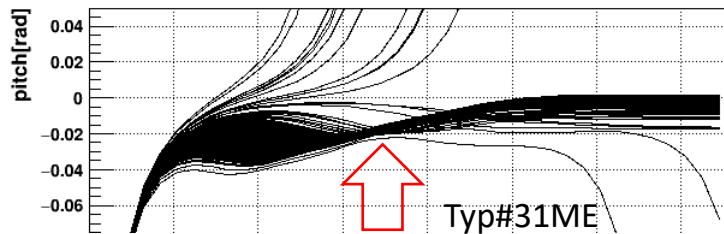
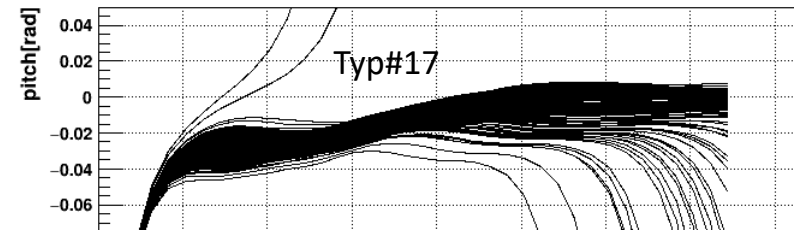
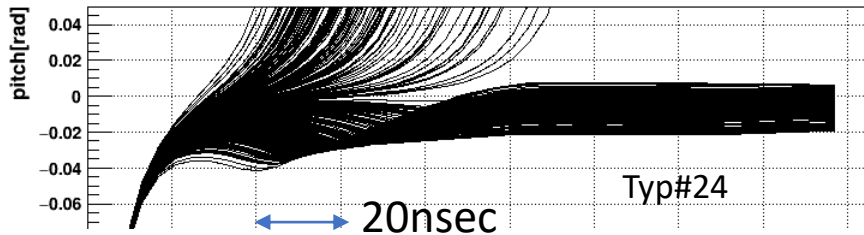
$$\text{Pitch angle} = z' = \text{asin}(v_z/v)$$

$$z_0 = - \int_{t_0}^{t_0 + \pi/\omega} v_z(t) dt$$

z-z' distribution
→ ΣBL

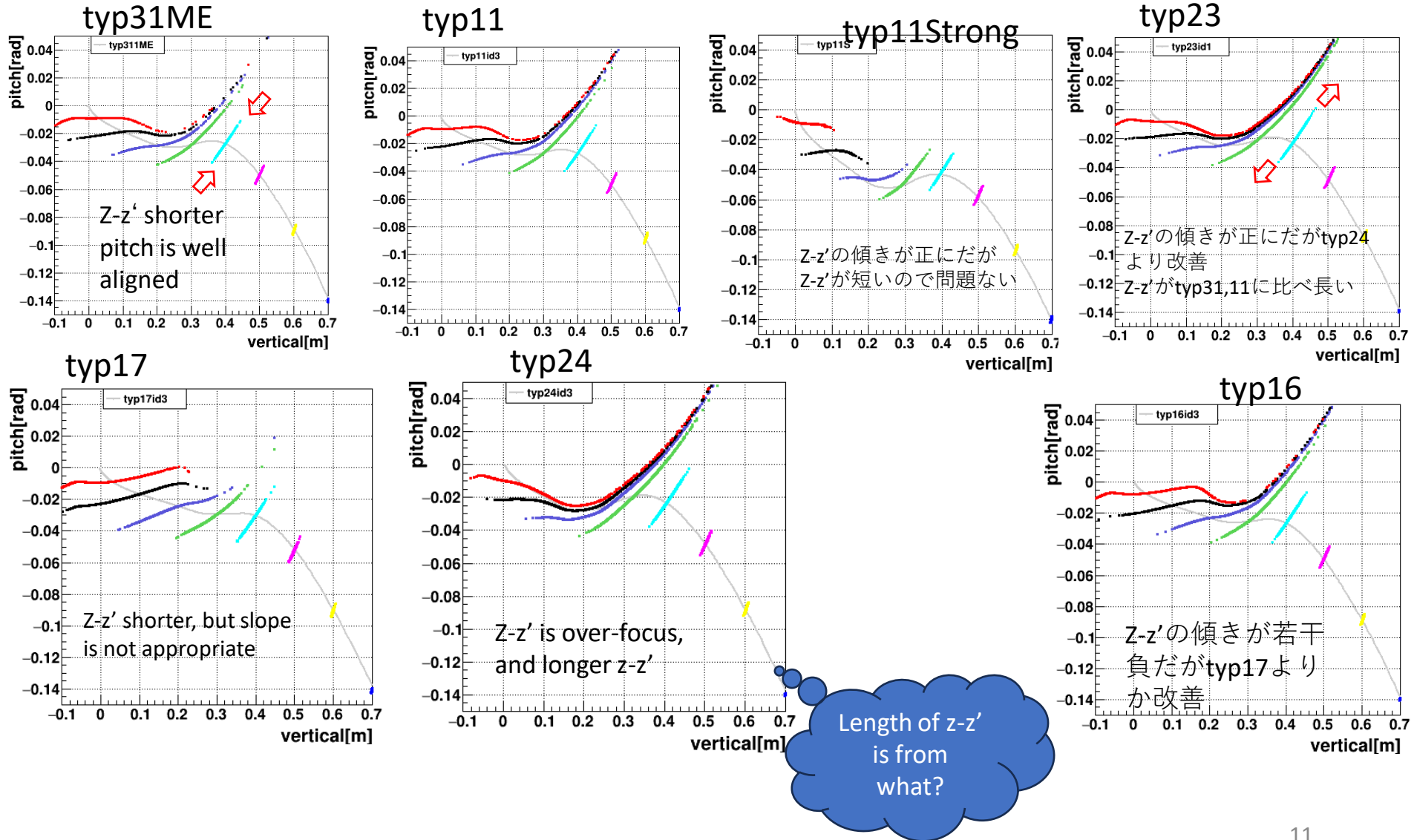
To get smaller z' distribution, control pitch angle “waist” is the key

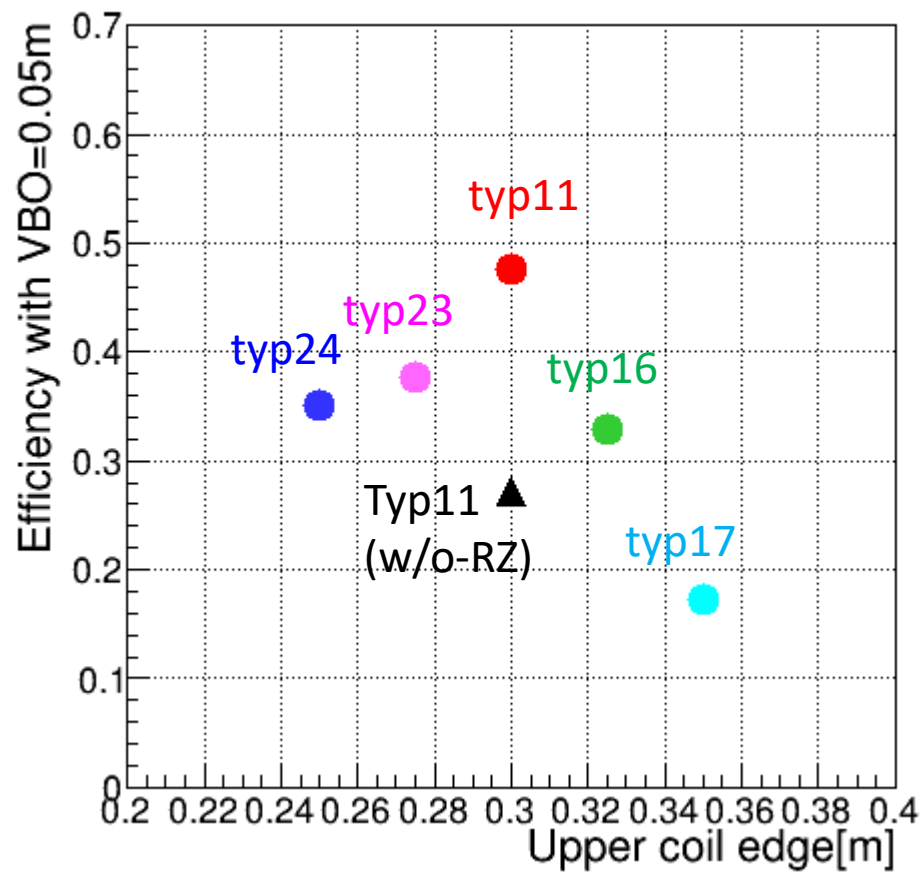
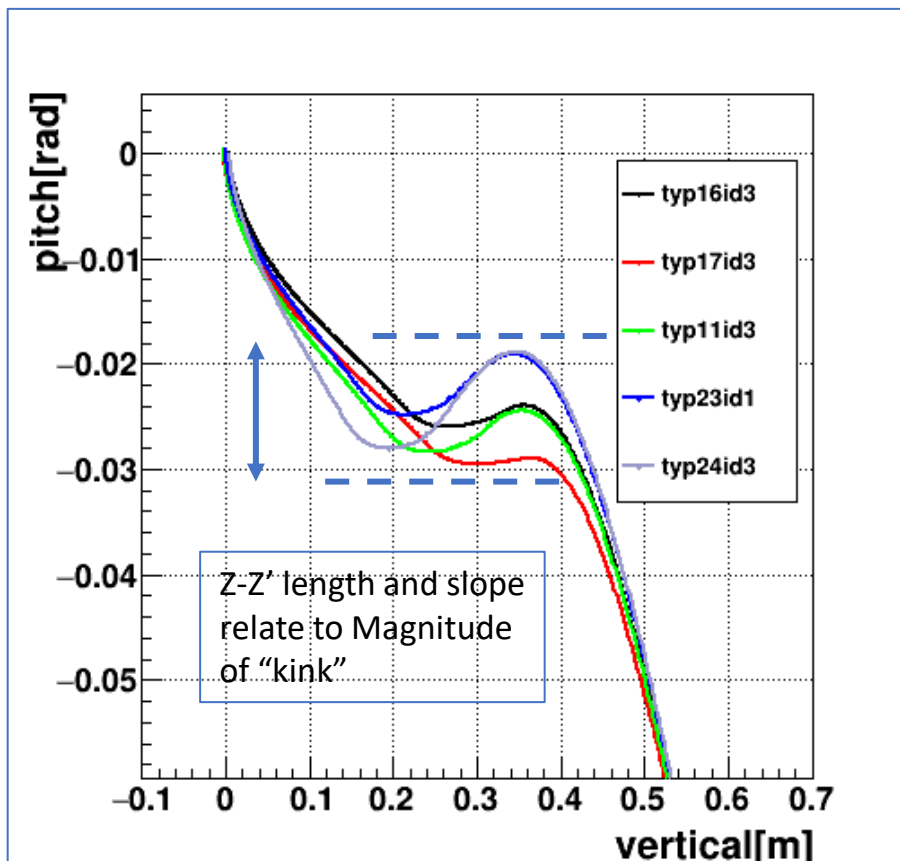
No working eigen vector



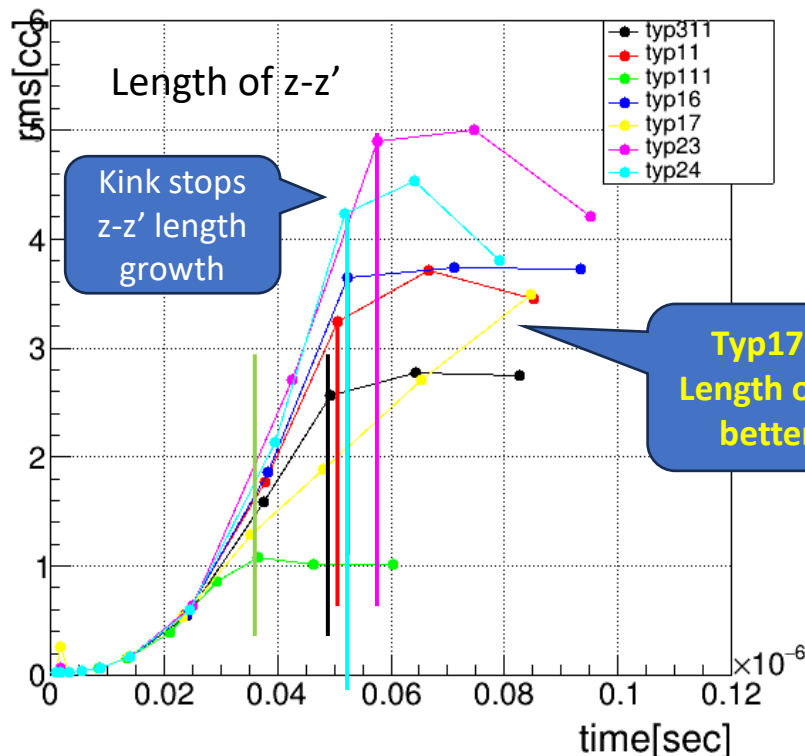
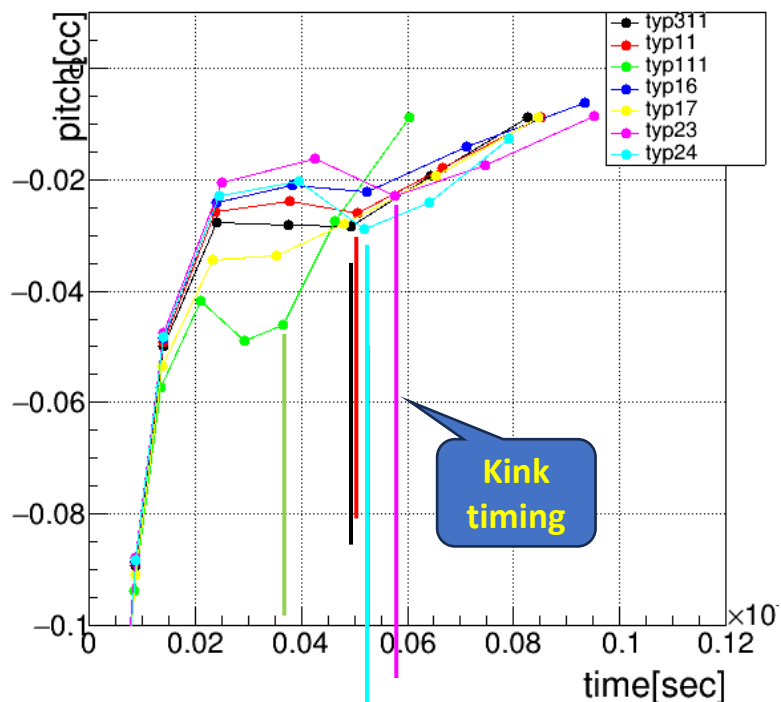
$Z < 0.1m$, pitch angle can't be controlled well, therefore it is better to set aligned the same pitch angle by $z \sim 0.1m$.

Kink-shape can control pitch's waist and make pitch angle flat at the end of the kick





“kink” can control the length of z-z' and slope



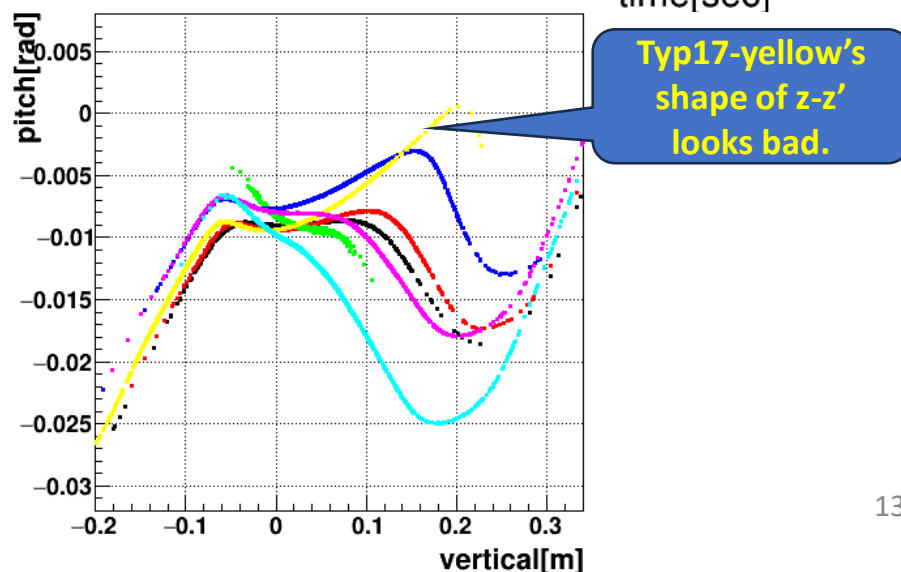
Tips for better injection efficiency

- Shorter z-z'
 - Z' ~ const
- (the same pitch angle, when the kink is over)

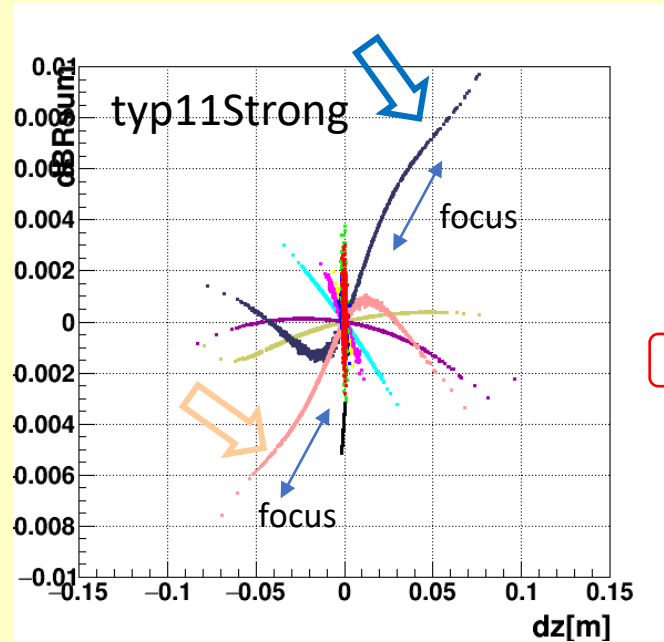
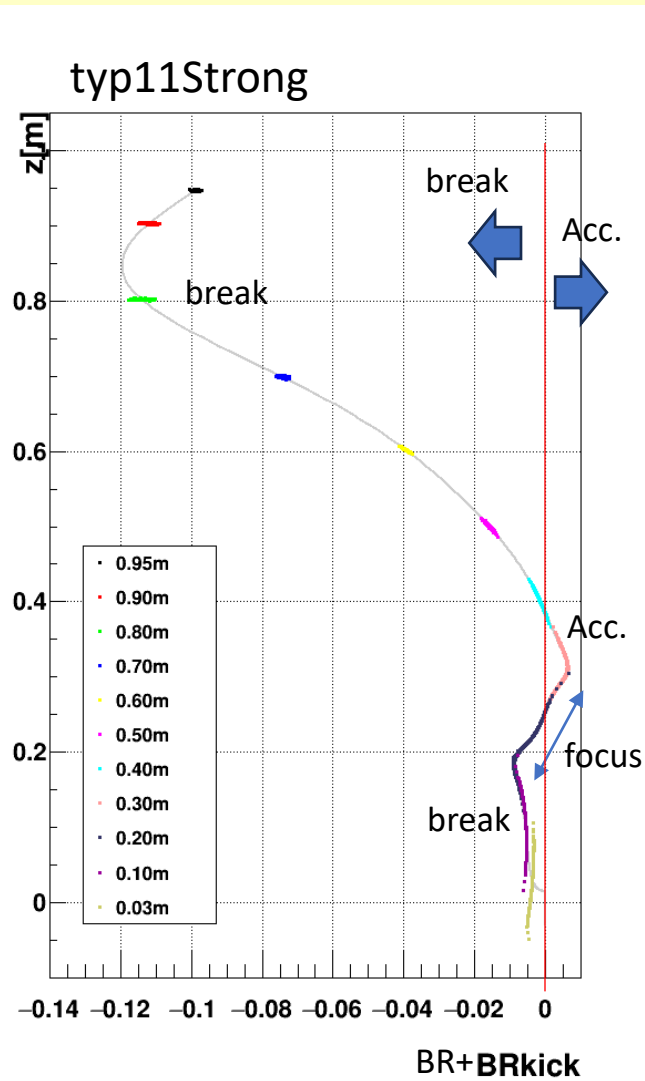


Guide a beam to kink point ASAP

- Bigger pitch angle with short time-flight to the pitch point= pass through fringe volume.

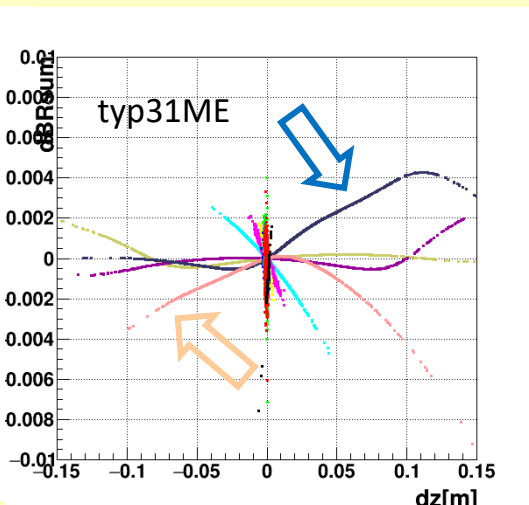
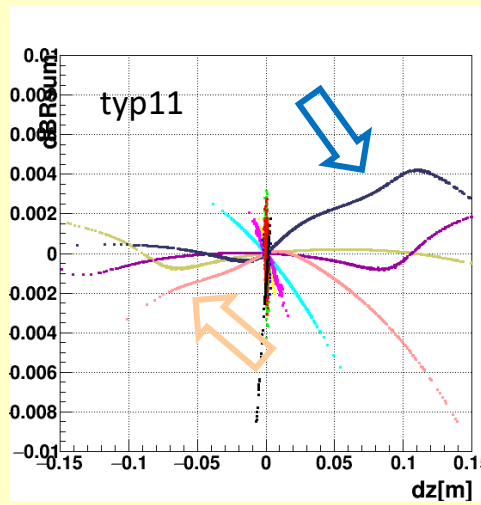


$dBR/dz \Rightarrow$ positive(negative) is focus (defocus)

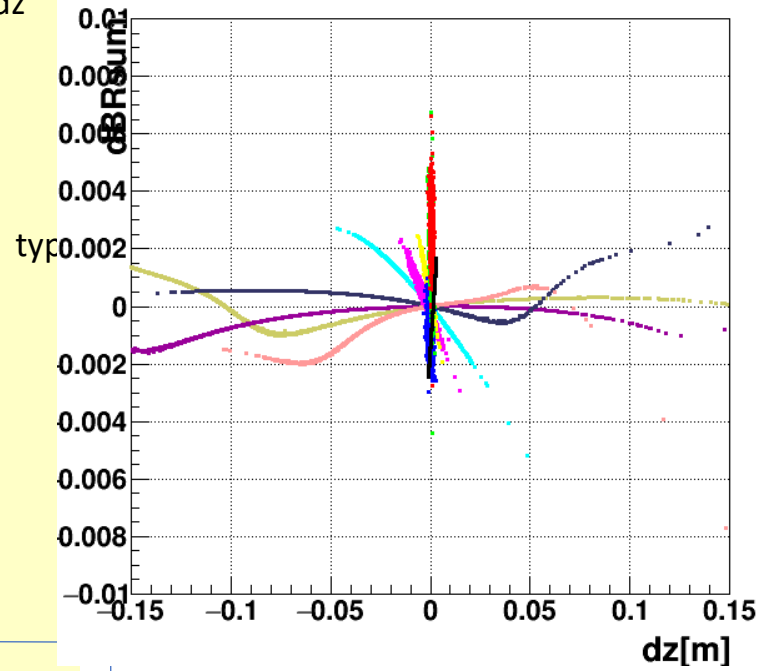


- 0.95m
- 0.90m
- 0.80m
- 0.70m
- 0.60m
- 0.50m
- 0.40m
- 0.30m
- 0.20m
- 0.10m
- 0.03m

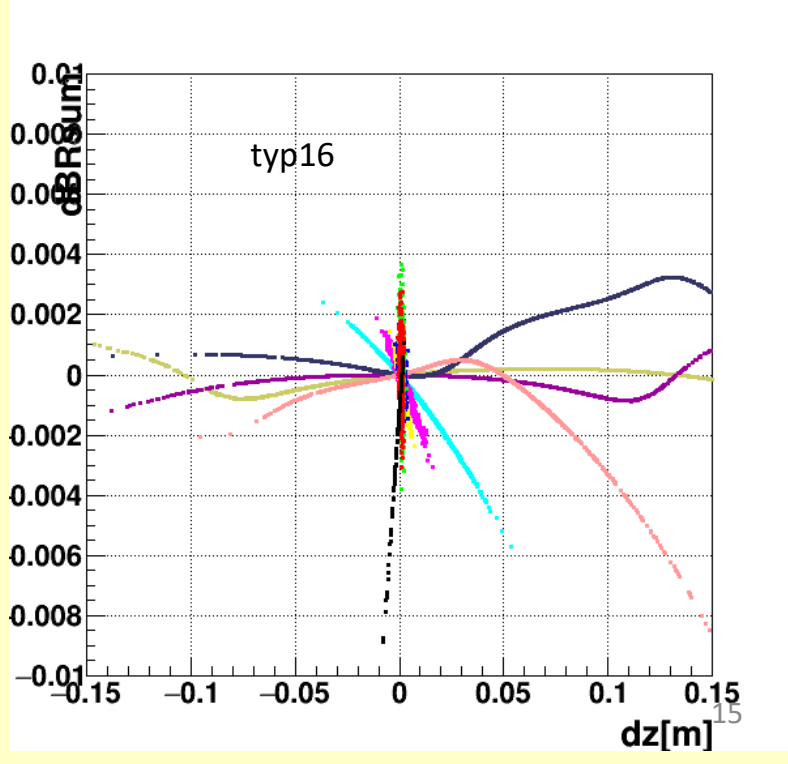
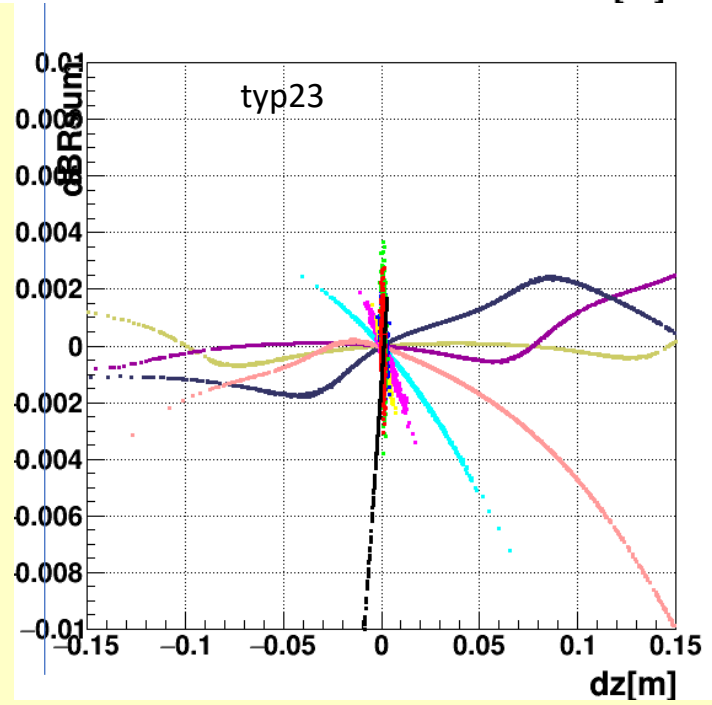
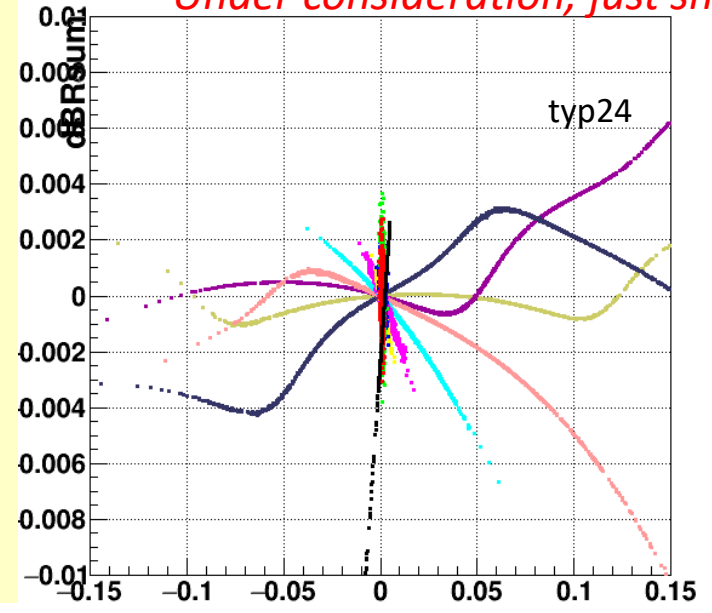
$z \sim 0.2 \sim 0.3$ を滑らかにつなぐ dBR/dz が鍵?



dBR/dz



Under consideration, just showing



Typ11 → vacuum bessel → typ31ME

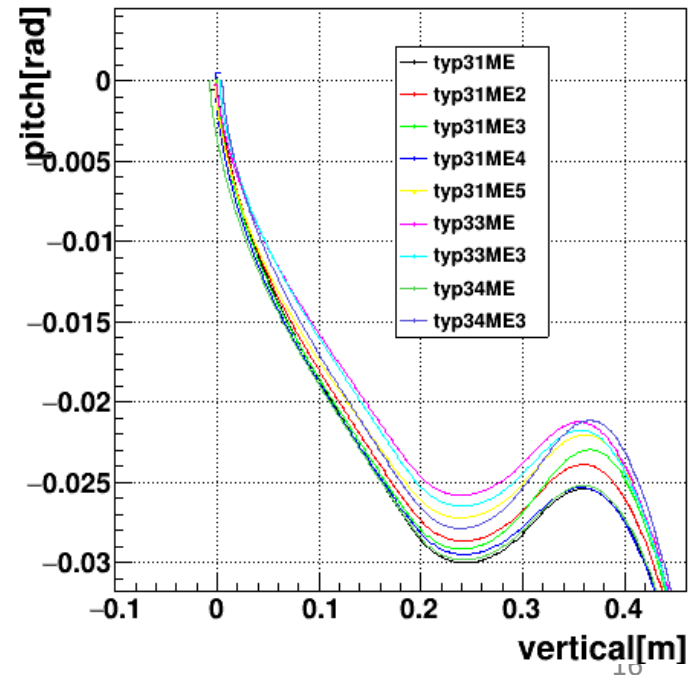
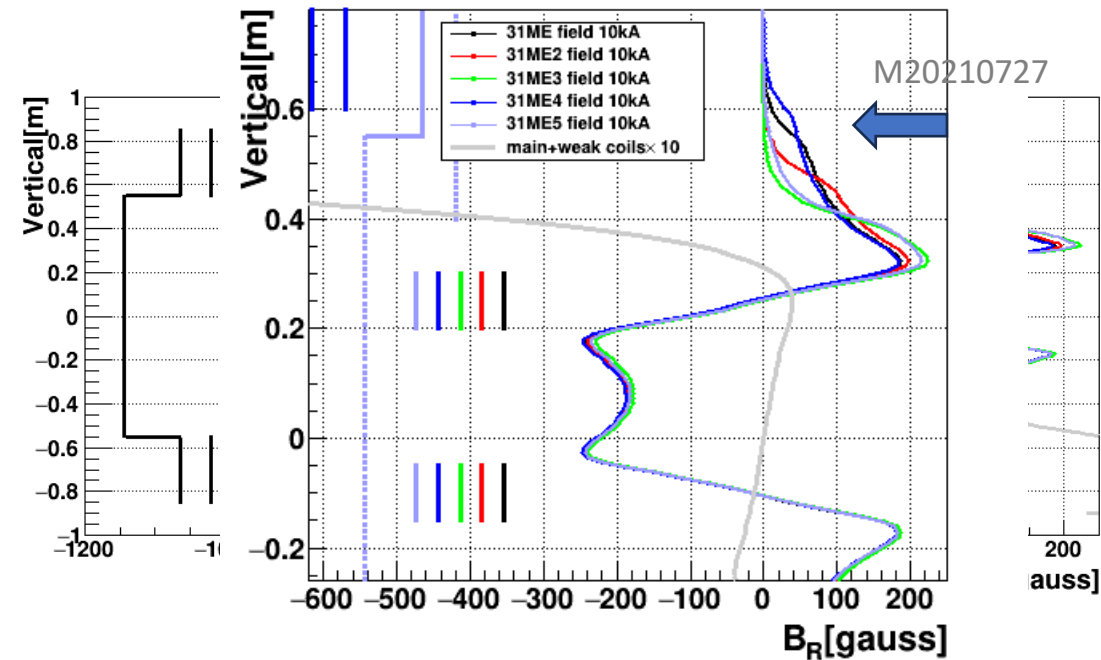
目的：真空容器の形状で上コイル付近の収束磁場分布形状を変えて、よりベターな条件を探す。

Table Parameters for Kicker field conceptual design (+/- 500A)

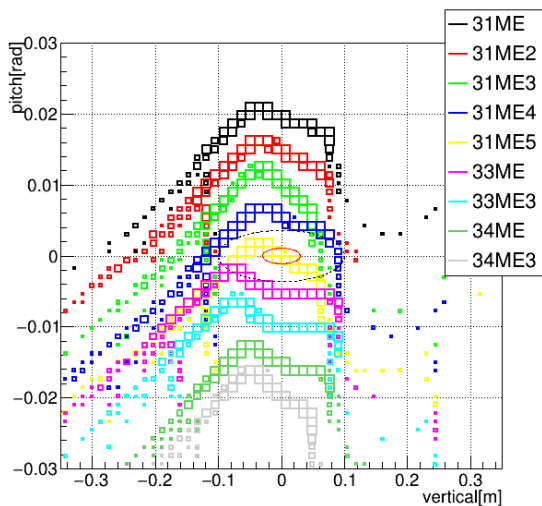
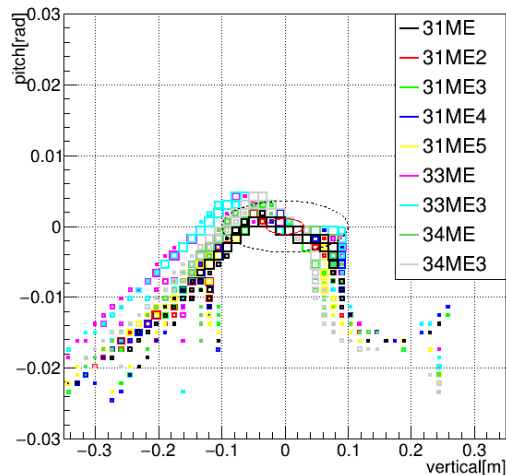
Parts	Parameter	Meaning	Type- →	31ME	31ME-2	31ME-3	31ME-4	31ME-5	33ME	33ME-3	34ME	34ME-3
Duct & Vessel wall	DZHI	Beam duct end height (Inner)		0.550	0.4750	0.400	0.600	0.400	0.550	0.400	0.550	0.400
	DZHO	Beam duct end height (Outer)		0.550	0.4750	0.400	0.600	0.550	0.550	0.400	0.550	0.400
	VZH	Vertical height of vessel ceiling		0.550	0.4750	0.400	0.600	0.550	0.550	0.400	0.550	0.400
	RD	Inner radius of beam duct		0.412	0.412	0.412	0.412	0.412	0.412	0.412	0.412	0.412
	RW	Outer radius of beam duct		0.300	0.300	0.300	0.300	0.300	0.300	0.300	0.300	0.300
Coil conductors	CZtop	Z height of top coil center		0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250
	CZbot	Z height of bottom coil center		-0.100	-0.100	-0.100	-0.100	-0.100	-0.150	-0.150	-0.120	-0.120
半径方向磁場BR強度	B333-+175	R=0.333, Z=0.175mのBR		12.23	12.00	11.40	12.30	11.78	11.54	10.67	11.92	11.07
	B333-+050	R=0.333, Z=0.050mのBR		9.54	9.44	9.13	9.59	9.35	7.65	7.19	8.67	8.23
	B333-0	R=0.333, Z=0.0mのBR		11.39	11.31	11.06	11.43	11.26	8.35	7.97	10.04	9.67
	B333--050	R=0.333, Z=-0.050mのBR		10.17	10.15	9.96	9.59	10.12	10.56	10.22	11.97	11.65

typ31ME → typ33ME, typ34ME
下コイルの位置を若干ずらし、z-z'形状への影響を確認する。

赤字数値はType-31MEのものである。Type-32はCZtopを0.29mとしたもので既提示、表中の数値の単位はm
コイル導体は5mm幅、10cm高さで、端部は2.5mm半径円弧の形状、上表では中心位置を変更している
31MEでは下側コイルの中心CZbotは-0.100m, 33MEは下側コイルの中心をCZbot=-0.15m, 34MEではCZbot=-0.120mとした。
33MEに比べ34MEでは蓄積領域のBRが強い。33MEでは、BR成分が弱くなっている。

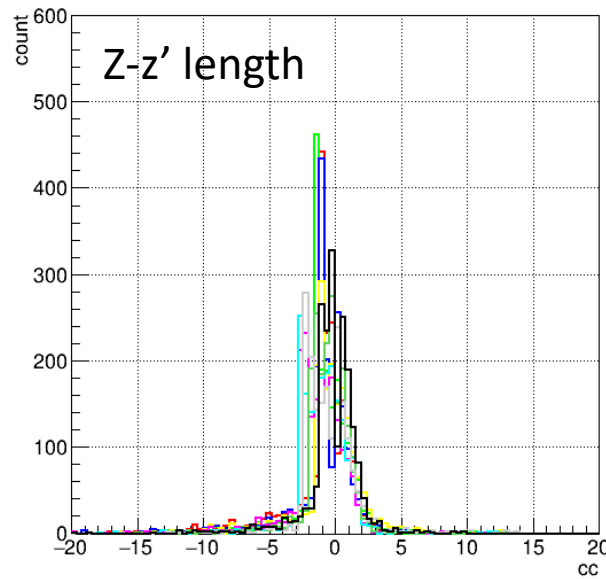
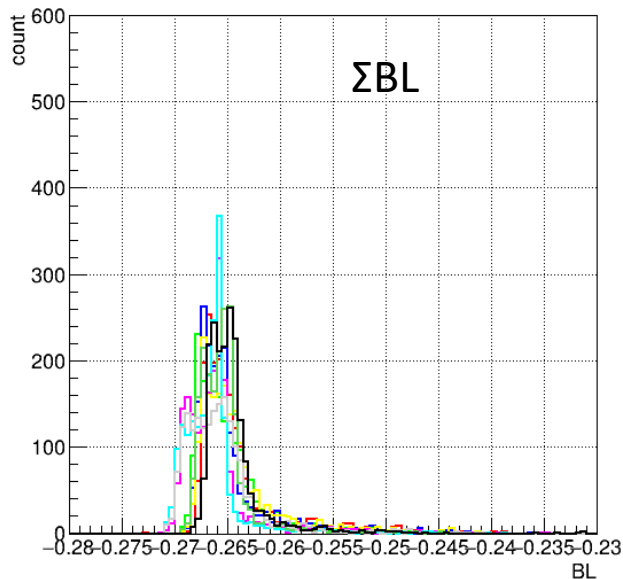


typ11typ31ME is better than typ11



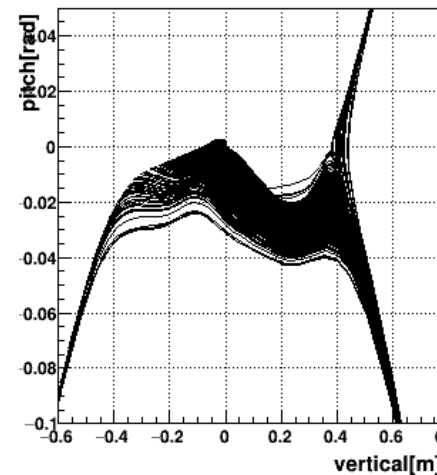
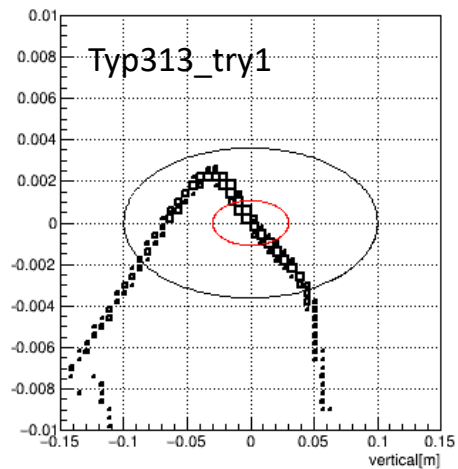
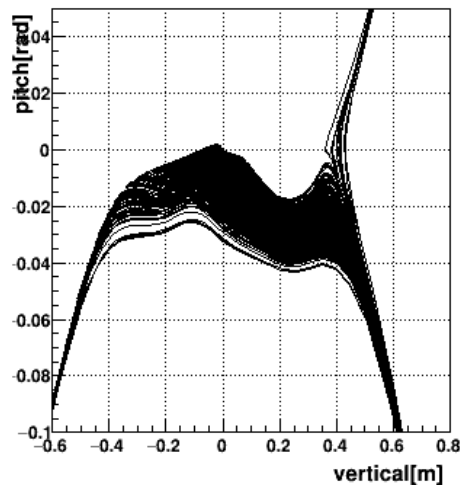
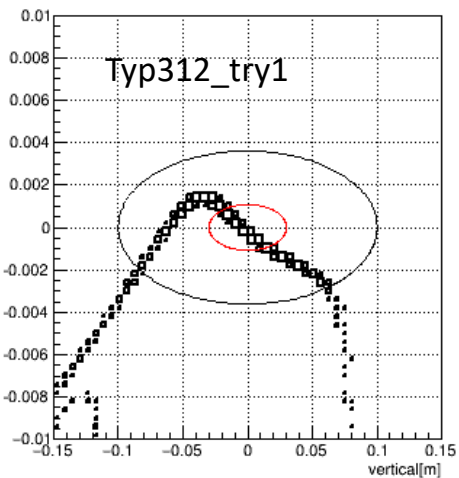
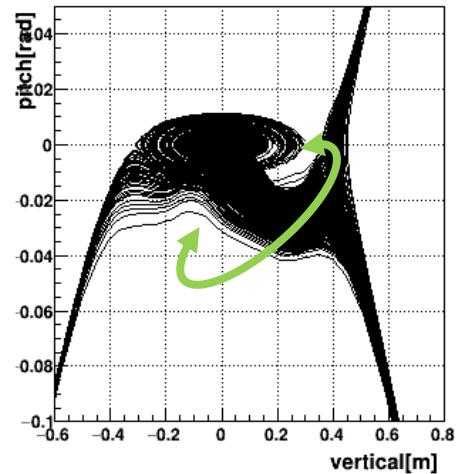
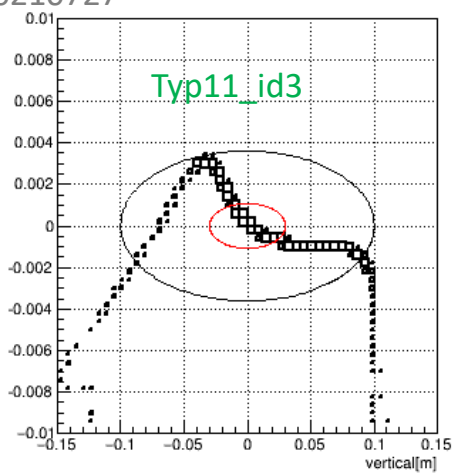
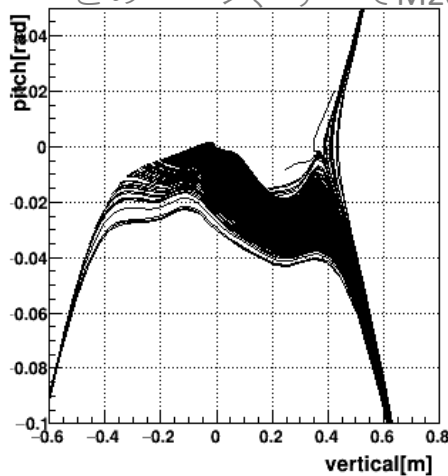
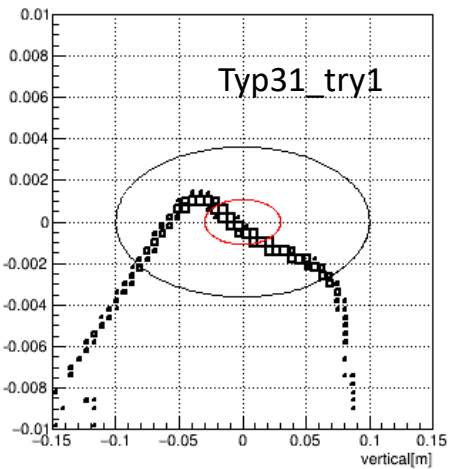
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ratio=0.434224	rms=0.004077
ratio=0.362468	rms=0.003845
ratio=0.411402	rms=0.003263
ratio=0.510529	rms=0.002747
ratio=0.420863	rms=0.003694

Σ BL \circ RMS

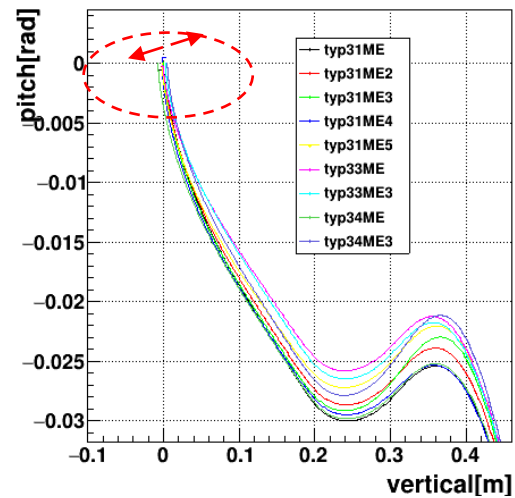
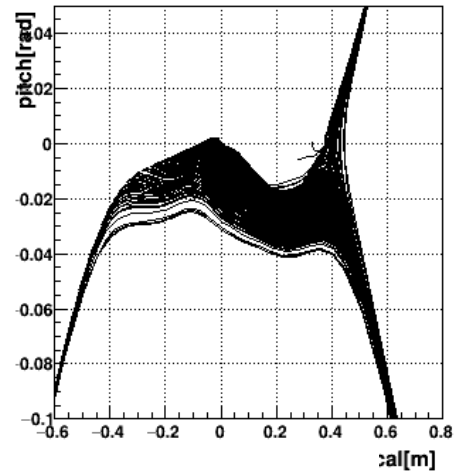
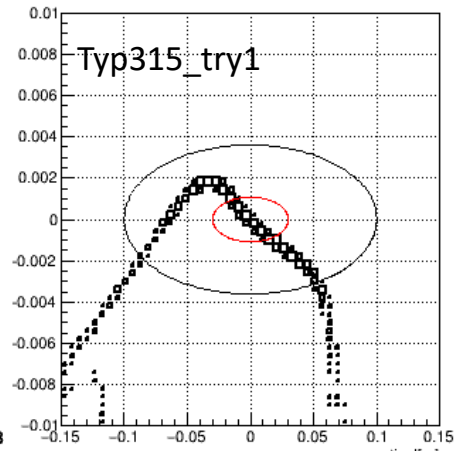
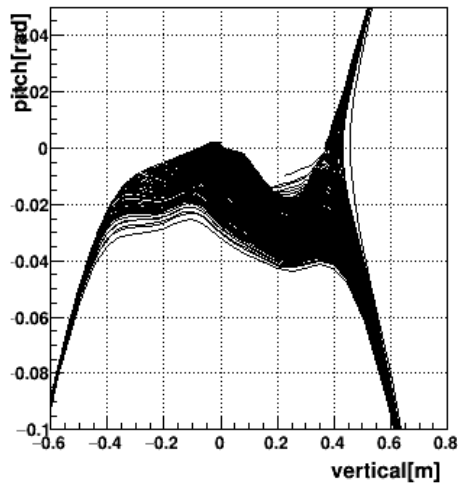
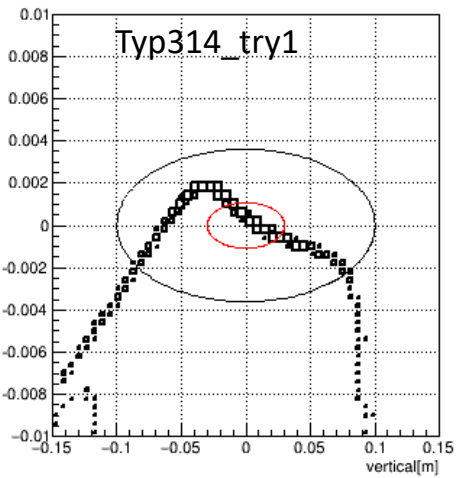


Ogawa-san is also checked this topics independently. See, whether we agree or not.

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